

DIFFRACTION OPTICAL ELEMENT

BACKGROUND OF THE INVENTION

Field of the Invention

5 This invention relates to a diffraction optical element, and particularly to a diffraction optical element suitable for use in a light including a plurality of wavelengths, or a wide-band light, and an optical system using the same.

10 Related Background Art

 In contrast with a conventional method of decreasing chromatic aberration by a combination of glass materials, a method of providing a diffraction optical element (hereinafter referred to also as the 15 diffraction grating) having the diffracting action on a lens surface or a portion of an optical system to thereby decrease chromatic aberration is disclosed in literature such as SPIE, Vol. 1354, International Lens Design Conference (1990), Japanese Patent Application 20 Laid-Open No. 4-213421, Japanese Patent Application Laid-Open No. 6-324262 and U.S. Patent No. 5,044,706. This method utilizes the physical phenomenon that in a refracting surface and a diffracting surface in an optical system, chromatic aberration for rays of light 25 of a certain reference wavelength appears in opposite directions. Further, such a diffraction optical element can also be given an effect like that of an

aspherical lens by the period of the periodic structure thereof being changed, and has a great effect in reducing aberrations.

Here, in refraction, a ray of light is a ray of light still after refraction, whereas in diffraction, a ray of light is divided into a plurality of orders. So, when a diffraction optical element is used as a lens system, it is necessary to determine the grating structure so that a light beam of a wavelength area used may concentrate in a particular order (hereinafter referred to also as the "design order"). When a light concentrates in the particular order, the intensity of the other rays of diffracted light becomes low, and when the intensity is zero, the diffracted light thereof becomes null.

Therefore, when the aberrations of an optical system are to be corrected by a diffraction optical element, it becomes necessary to that element that the diffraction efficiency of a ray of light of the design order be sufficiently high in the entire wavelength area used. Also, when there are present rays of light having the other diffraction order than the design order, those rays of light are imaged at locations discrete from the location for the ray of light of the design order and therefore become flare light.

Accordingly, in an optical system using the diffraction effect, it is important to give sufficient

consideration also to the spectral distribution of the diffraction efficiency at the design order and the behavior of the rays of light of the other diffraction orders than the design order.

When a diffraction optical element 201 having a diffraction grating 204 comprising a layer provided on a substrate 202 as shown in Fig. 16 of the accompanying drawings is formed on a certain surface, the characteristic of diffraction efficiency for the particular diffraction order is shown in Fig. 17 of the accompanying drawings. Hereinafter, the value of the diffraction efficiency is the rate of the quantity of each diffracted light to the whole transmitted light beam, and is a value in which the reflected light or the like on the boundary surface of the diffraction grating is not taken into consideration because it is complex to describe. In Fig. 17, the axis of abscissas represents wavelength and the axis of ordinates represents diffraction efficiency. The diffraction optical element 201 is designed such that in the first diffraction order (solid line in the figure), the diffraction efficiency becomes highest for the wavelength area used. That is, the design order is the first order. Further, the diffraction efficiency for the diffraction orders in the vicinity of the design order (zero order and second order which are first order \pm one order) is also shown. At the design order,

the diffraction efficiency becomes highest for a certain wavelength (hereinafter referred to as the "design wavelength") and gradually becomes lower for the other wavelengths. The decrement in the
5 diffraction efficiency at this design order is the increment in the diffraction efficiency at the other orders than the design order, and diffracted lights of the other orders than the design order become flare lights. Also, when a plurality of diffraction optical
10 elements are used, particularly a reduction in the diffraction efficiency at the other wavelengths than the design wavelength also leads to a reduction in transmittance.

A construction which can decrease such a reduction
15 in the diffraction efficiency is disclosed in Japanese Patent Application Laid-Open No. 9-127322. This, as shown in Fig. 18 of the accompanying drawings, optimally selects three kinds of different materials and two kinds of different grating thicknesses, and
20 disposes them in proximity at an equal pitch distribution to thereby realize high diffraction efficiency in the entire visible area, as shown in Fig. 19 of the accompanying drawings.

Also, the assignee of the application presents in
25 Japanese Patent Application Laid-Open No. 10-133149 a diffraction optical element which can decrease any reduction in diffraction efficiency. Fig. 20 of the

accompanying drawings shows the construction presented in the above-mentioned proposition, and it has a laminated cross-sectional shape in which two layers are stacked. High diffraction efficiency is realized by
5 optimizing the refractive indices of materials forming the two layers, the spectral characteristic and the thickness of each grating.

If a diffraction optical element is provided in an optical system, light beams of various angles of views
10 usually enter the diffraction optical element. Therefore, if a diffraction optical element having a diffraction grating provided on a flat plate is used in an optical system, the angle of incidence of a light beam onto the diffraction optical element is changed by
15 the angles of view, and the diffraction efficiency of diffracted light at the design order comes to be changed by the angles of view.

In particular, a laminated diffraction optical element, as compared with the prior-art single-layer
20 diffraction optical element shown in Fig. 16, tends to become greater in the thickness of the grating.

Therefore, a laminated diffraction optical element formed on a flat plate, when used in an optical system having an angle of view, has its diffraction efficiency
25 greatly reduced by the eclipse or the like of a light beam on the edge surface of the grating.

In contrast, it would occur to mind to use a

diffraction optical element having a diffraction grating on a curved surface in an optical system having an angle of view. In this case, when the diffraction optical element is disposed, for example, more adjacent to the object side than a stop, a change in the angle of incidence of a light beam onto the diffraction optical element may be reduced depending on a change in the angle of view by the diffraction grating being provided on a curved surface which is concave relative to the stop.

Actually, however, unless the shape of the grating when a diffraction optical element having laminated structure is formed on a curved surface is made appropriate, high optical performance equal to that of a diffraction optical element of laminated structure formed on a flat surface will not be obtained in some cases.

SUMMARY OF THE INVENTION

The present invention has as its object the provision of a diffraction optical element which, even when used in an optical system having an angle of view, has a small change in diffraction efficiency depending on the angle of view, and an optical system using the same.

A first diffraction optical element of the present invention is a diffraction optical element having

structure in which at least two diffraction gratings formed of at least two kinds of materials differing in dispersion are laminated, and having its diffraction efficiency of a particular order enhanced in the
5 wavelength area used, characterized in that at least two of the diffraction gratings are formed on a curved surface and adjacent to each other, and these two adjacent diffraction gratings are of a curved surface shape in which curved tip planes in which the tips of
10 respective grating portions are ranged are equal to each other.

A second diffraction optical element of the present invention is a diffraction optical element having structure in which at least two diffraction gratings formed of at least two kinds of materials differing in dispersion are laminated, and having its diffraction efficiency of a particular order enhanced in the wavelength area used, characterized in that at least two of the diffraction gratings are formed on a
15 curved surface and adjacent to each other, and a curved tip plane in which the tips of the grating portion of one of these two adjacent diffraction gratings are ranged and a groove bottom curved surface in which the groove bottoms of the grating portion of the other
20 diffraction grating are ranged are of an equal curved surface shape.
25

A third diffraction optical element of the present

invention is a diffraction optical element having
structure in which at least two diffraction gratings
formed of at least two kinds of materials differing in
dispersion are laminated, and having its diffraction
5 efficiency of a particular order enhanced in the
wavelength area used, characterized in that at least
two of the diffraction gratings are formed on a curved
surface and adjacent to each other, and these two
adjacent diffraction gratings are such that a line
10 linking the tips of the opposed grating portions
thereof is substantially parallel to an optical axis.

A fourth diffraction optical element of the
present invention is a diffraction optical element
having structure in which a plurality of diffraction
15 gratings formed of at least two kinds of materials
differing in dispersion are laminated, and having its
diffraction efficiency of a particular order enhanced
in the wavelength area used, characterized in that two
adjacent ones of the plurality of diffraction gratings
20 satisfy

$$\alpha \leq \beta,$$

where β represents the angle formed between the grating
edge of the grating portion thereof and the grating
surface of the grating portion, and α represents the
25 angle formed by the grating surface with respect to the
surface normal of a curved tip plane at a position
whereat the curved tip plane in which the tips of the

grating portion are ranged and the tips intersect with each other.

A fifth diffraction optical element of the present invention is a diffraction optical element having
5 structure in which a plurality of diffraction gratings formed of at least two kinds of materials differing in dispersion are laminated, and having its diffraction efficiency of a particular order enhanced in the wavelength area used, characterized in that the grating thickness of the grating portions of the diffraction gratings is such that the length of the grating thickness in a direction parallel to the surface normal of a curved tip plane in which the tips of the grating portions are ranged at a position whereat the curved
10 tip plane and the tips intersect with each other is constant.
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A sixth diffraction optical element of the present invention is a diffraction optical element having structure in which at least two diffraction gratings formed of at least two kinds of materials differing in dispersion are laminated, whereby the diffraction efficiency of a particular order (design order) is enhanced in the entire wavelength area used, characterized in that at least two of the diffraction gratings are formed on a curved surface and adjacent to each other, and these two adjacent diffraction gratings
20 are equal to each other in the center of curvature of
25

the curved tip plane of each grating portion thereof in which the most proximate tips of the gratings are ranged.

A seventh diffraction optical element of the
5 present invention is a diffraction optical element having laminated grating structure in which at least two diffraction gratings formed of at least two kinds of materials differing in dispersion are stacked in proximity to one another, and having its diffraction
10 efficiency of a particular order enhanced in the wavelength area used, characterized in that two of the diffraction gratings are formed on a curved surface and adjacent to each other, and the grating spacing between these two adjacent diffraction gratings is equal over
15 the range of use.

Each of the aforescribed elements has a form in which the plurality of laminated diffraction gratings are joined together in the non-grating area of each diffraction grating.

20 Each of the aforescribed elements has a form in which the plurality of laminated diffraction gratings include a diffraction grating differing in the direction of the grating shape from at least one other diffraction grating.

25 Each of the aforescribed elements has a form in which the wavelength area used is a visible range.

Each of the aforescribed elements has a form in

which at least one of the plurality of diffraction gratings is such that the material forming the diffraction grating is the same as the material forming a substrate on which the diffraction gratings are provided.

5 Each of the aforedescribed elements has a form in which a substrate on which the diffraction gratings are formed has lens action.

10 Each of the aforedescribed elements has a form in which it is formed on the cemented surface of a cemented lens.

15 The optical system of the present invention is characterized in that it uses any one of the aforedescribed elements and the aforedescribed forms of diffraction optical element.

20 The optical system is an imaging optical system or an observation optical system.

BRIEF DESCRIPTION OF THE DRAWINGS

20 Fig. 1 is a schematic view of the essential portions of a diffraction optical element according to Embodiment 1 of the present invention.

25 Fig. 2 is a cross-sectional view of the essential portions of a diffraction grating in Embodiment 1 of the present invention.

Fig. 3 is an illustration of the diffraction efficiency of the diffraction optical element according

to Embodiment 1 of the present invention.

Fig. 4 is an illustration of grating pitch.

Fig. 5 is an illustration of the curved surface shape of the tip of a diffraction grating.

5 Fig. 6 is an illustration of the curved surface shape of the tip of a diffraction grating.

Fig. 7 is an illustration of the curved surface shape of the tip of a diffraction grating.

10 Fig. 8 is an illustration of the grating pitch and curved surface shape of the diffraction grating.

Fig. 9 is an illustration of the grating edge shape.

Fig. 10 is an illustration of the thickness of the grating.

15 Fig. 11 is an illustration of a one-dimensional diffraction optical element according to Embodiment 1 of the present invention.

20 Fig. 12 is a schematic view of the essential portions of a diffraction optical element according to Embodiment 2 of the present invention.

Fig. 13 is a schematic view of the essential portions of a diffraction optical element according to Embodiment 3 of the present invention.

25 Fig. 14 shows a photo-taking optical system according to Embodiment 4 of the present invention.

Fig. 15 shows an observation optical system according to Embodiment 5 of the present invention.

Fig. 16 is an illustration of the grating shape (triangular wave shape) of a diffraction optical element according to the prior art.

5 Fig. 17 is an illustration of the diffraction efficiency of the diffraction optical element according to the prior art.

Fig. 18 is an illustration of the cross-sectional shape of the diffraction grating of a laminated type diffraction optical element according to the prior art.

10 Fig. 19 is an illustration of the diffraction efficiency of the laminated type diffraction optical element according to the prior art.

15 Fig. 20 is an illustration of the cross-sectional shape of the diffraction grating of the laminated type diffraction optical element according to the prior art.

Fig. 21 is an illustration of the cross-sectional shape of a diffraction optical element according to the prior art formed on a flat plate.

20 Fig. 22 is an illustration of the diffraction efficiency of the diffraction optical element according to the prior art formed on a flat plate.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Fig. 1 is a front view and a side view of the
25 essential portions of the diffraction optical element of the present invention, and Figs. 2 and 6 are partial cross-sectional views of the element 1 of Fig. 1 along

the line 2-2 of Fig. 1.

Referring to Fig. 1, reference numeral 1 designates a diffraction optical element comprising the diffraction grating 6 of a first diffraction optical element 2 and the diffraction grating 7 of a second diffraction optical element 3 which are proximate and opposed to each other. The diffraction gratings 6 and 7 constituting the diffraction optical element 1 comprise concentric circular grating shapes and have lens action. Also, the two adjacent diffraction gratings 6 and 7 provide curved surfaces (curved tip planes) 9 and 10 when the tips 6b (7b) of grating portions 6-1 (7-1) are ranged. The two curved tip planes 9 and 10 are of equal curved surface shapes. O denotes an optical axis.

Fig. 2 is a view of the diffraction gratings 6 and 7 considerably deformed in the direction of depth of the gratings. The diffraction optical element 1 is of a construction in which the first diffraction optical element 2 having the diffraction grating 6 formed on the surface of a substrate 4 and the second diffraction optical element 3 having the diffraction grating 7 formed on the surface of a substrate 5 are proximate to each other with air 8 therebetween. Further, the surfaces of the substrates 4 and 5 on which the diffraction gratings 6 and 7 are formed and the surfaces opposite thereto are curved surfaces, and the

substrates 4 and 5 themselves have the action as a refracting lens. In Fig. 2, the reference numerals 9 and 10 designate the curved tip planes of the diffraction gratings 6 and 7.

5 The diffraction efficiency of the diffraction optical element will first be described.

A diffraction optical element 201 of the ordinary transmission type as shown in Fig. 16 has a layer of diffraction grating 204, and the condition under which 10 diffraction efficiency becomes maximum at the design wavelength λ_0 is that when a light beam enters a diffraction grating 204 (diffraction surface) perpendicularly thereto, the difference in optical 15 light path difference between the mountain and valley of the diffraction grating 204 becomes integer times as great as the wavelength, and this can be represented by the following expression:

$$(n_{01} - 1)d = m\lambda_0, \quad (1)$$

where n_{01} represents the refractive index of the 20 material of the diffraction grating at a wavelength λ_0 , d represents the thickness of the grating, and m represents the diffraction order. Fig. 17 shows the diffraction efficiency of the diffraction optical element 201 at this time.

25 On the other hand, a diffraction optical element 301 having two or more layers of diffraction gratings 306, 307 as shown in Fig. 21, in order to make it act

as a diffraction grating through all layers, is determined so that the differences in the optical light path length between the mountains and valleys of the diffraction gratings 306, 307 may be found and the 5 total thereof over all layers may be integer times as great as the wavelength. In Fig. 21, the reference numerals 304 and 305 designate substrates, and the reference numeral 308 denotes an air layer. The conditional expression under which the diffraction 10 efficiency when a light beam enters the diffraction optical element 301 of laminated structure shown in Fig. 21 perpendicularly thereto becomes maximum is

$$\pm (n_{o1} - 1)d1 \pm (n_{o2} - 1)d2 = m\lambda_0, \quad (2)$$

where n_{o1} represents the refractive index of the 15 material of the first diffraction grating 306 at the wavelength λ_0 , n_{o2} represents the refractive index of the material of the second diffraction grating 307 at the wavelength λ_0 , and $d1$ and $d2$ represent the grating thickness of the first diffraction grating 306 and the 20 second diffraction grating 307, respectively. Here, when the direction of diffraction is made such that the downward diffraction from 0-order diffracted light in Fig. 21 is a positive diffraction order and the upward diffraction from 0-order diffracted light is a negative 25 diffraction order, the signs of increase and decrease in each layer in expression (2) become such that the case of a grating shape (in the figure, the diffraction

grating 307) in which as shown, the grating thickness increases from up to down is positive, and the case of a grating shape (in the figure, the diffraction grating 306) in which conversely, the grating thickness 5 increases from down to up is negative. A specific example will hereinafter be cited and described.

First, the following construction is adopted as the first diffraction optical element 302. The material forming the diffraction grating 306 is 10 ultraviolet ray setting resin ($n_d = 1.635$, $v_d = 23.0$), and the thickness d_1 of the grating is $6.9 \mu\text{m}$. Likewise, the following construction is adopted as the second diffraction optical element 303. The material forming the diffraction grating 307 is ultraviolet ray 15 setting resin C001 ($n_d = 1.524$, $v_d = 50.8$) produced by Dainippon Ink Chemical Industry Ltd., and the thickness d_2 of the grating is $9.5 \mu\text{m}$. The diffraction efficiency of the first order diffracted light and zero order and second order in the vicinity thereof in this 20 construction is shown in Fig. 22.

As can be seen from Fig. 22, the first order diffracted light maintains high diffraction efficiency in the entire visible range. It can also be seen that the diffraction efficiency of the zero order and second 25 order diffracted lights which are the neighboring orders of the first order diffracted light which is the design order is greatly reduced as compared with the

example of the prior art shown in Fig. 17.

Description will now be made of the shape of the diffraction optical element of the present invention having a diffraction grating formed on a curved surface. As the construction, it is to be understood that the above-mentioned diffraction grating is formed on a curved surface having a radius of curvature R (hereinafter referred to as the reference curved surface).

Description will first be made of the grating pitches of the diffraction gratings 6 and 7 of the first diffraction optical element 2 and the second diffraction optical element 3, respectively. As regards the grating pitch of the diffraction grating when formed on a curved surface, it is preferable that the grating pitch distributions at the positions of the tips 6b and 7b of those grating portions 6-1 and 7-1 of the diffraction gratings 6 and 7 adjacent to each other which are most proximate become substantially equal to each other. That is, design is made such that a segment linking the tips 6b and 7b of the grating portions 6-1 and 7-1 opposed to each other is substantially parallel to the optical axis O. Fig. 4 shows as a comparative example a diffraction optical element of such a combination in which only the grating pitch distributions at the positions of the tips of the gratings on the substrate side (in Fig. 4, the groove

bottoms 6c and 7c of the grating portions of the diffraction gratings 6 and 7) are equal to each other. In the ensuing illustrations, only the diffraction gratings are shown and particularly the substrate is
5 not shown.

In the construction shown in Fig. 4, a light beam propagating through an area represented by hatching A emerges from the grating portion 6-1 of the first diffraction grating 6, whereafter it does not enter a
10 corresponding grating portion 7-1, but enters a grating portion 7-2 adjacent to this grating portion 7-1. Accordingly, the light beam in the area of hatching A cannot obtain a desired optical light path length difference and is not converted into diffracted light
15 of the design order, but becomes unnecessary diffracted light of other order than the design order. Therefore, in the present embodiment, in order to reduce this unnecessary light beam, design is made such that as shown in Fig. 2, the grating pitch distribution at the
20 position P of the tip of the grating most proximate to the grating portion 7-1 of the grating 7 adjacent to the grating portion 6-1 becomes equal to the grating pitch distribution at the position of the tip of the grating portion 6-1.

25 Description will now be made of the shapes of surfaces (curved tip planes) 9 and 10 in which the tips of the grating portions 6-1 and 7-1 of the diffraction

gratings 6 and 7 of the first and second diffraction optical elements 2 and 3, respectively, are ranged.

In the diffraction optical element of Fig. 2, the shapes of the surfaces (curved tip planes) 9 and 10 in which the tips 6b and 7b of the grating portions 6-1 and 7-1 of the two adjacent diffraction gratings 6 and 7, respectively, are ranged are substantially equal to each other.

Fig. 5 shows as a comparative example a diffraction optical element 51 in which the shapes of only curved surfaces 4a and 5a in which the groove bottoms 6c and 7c of grating portions 6-1 and 7-1, respectively, are ranged are equal to each other. Here, a case where diffraction gratings 6 and 7 are formed on curved surfaces 4a and 5a of a radius of curvature R will be described as an example. In this case, the radii of curvature of curved tip planes 4b and 5b in which the tips 6b and 7b of the grating portions 6-1 and 7-1 of the diffraction gratings 6 and 7 are ranged change by an amount corresponding to the thickness of the grating, and the radius of curvature of the curved tip plane 4b of the first diffraction optical element 2 is $R-d_1$, and the radius of curvature of the curved tip plane 5b of the second diffraction optical element 3 is $R+d_2$. The spacing on the optical axis O between the curved tip planes 4b and 5b in which the tips 6b and 7b are ranged is defined as D_1 .

Here, as a specific numerical value example, the spacing between the diffraction gratings in the peripheral portions thereof when the radius of curvature R is 150 mm and the effective diameter of the 5 gratings is φ100 mm and the thickness d₁ of the grating is 9.5 μm and the thickness d₂ of the grating is 6.9 μm and the spacing D₁ is 3 μm is about 2.0 μm which is smaller by the order of 1.0 μm as compared with the central portion on the optical axis. This fluctuation 10 of the spacing is an amount which cannot be neglected when it is taken into account that the thickness of the grating is of the order of several μm. Accordingly, in order to eliminate the fluctuation of this grating spacing (the spacing between the tip of a certain 15 grating portion and the tip of another grating portion opposed thereto) depending on the location, in the present embodiment, the shapes of the curved tip planes 9 and 10 in which the tips 6b and 7b of the grating portions 6-1 and 7-1 of the two adjacent diffraction 20 gratings 6 and 7 are ranged are made substantially equal to each other as shown in Figs. 2 and 6 (in Fig. 6, the both curved tip planes have the same radius of curvature R).

When as shown in Fig. 7, a diffraction optical 25 element 70 is comprised of first, second and third diffraction optical elements 71, 72 and 73, design is made such that a curved tip plane 71c in which the tips

71b of the grating portions 71a-1 of the diffraction gratings 71a of the element 71 are ranged and a groove bottom curved surface 72c in which the groove bottoms 72d of the grating portions 72a-1 of the diffraction gratings 72a of the element 72 adjacent to the element 71 are ranged are made into curved surfaces (radius of curvature R) equal in radius of curvature to each other. Also, design is made such that curved tip planes 72d and 73c in which the tips 72e and 73b of the grating portions 72a-1 and 73a-1 of the adjacent diffraction gratings 72a and 73a are ranged become curved surfaces (radius of curvature R-d2) equal in radius of curvature to each other. Here, which of the curved surfaces in which the tips of the gratings are ranged should be the reference curved surface is not particularly restricted.

The manner of determining the grating pitches of the diffraction gratings 6 and 7 and the surface shapes of the curved tip planes 9 and 10 thereof when the curved tip planes 9 and 10 in which the tips 6b and 7b of the most proximate grating portions 6-1 and 7-1 of the adjacent diffraction gratings 6 and 7 are ranged are separate from each other by D1 in the direction of the optical axis O will now be described in detail with reference to Fig. 8.

A curved surface 12 having a desired radius of curvature R is imaginarily disposed at the intermediate

position of the spacing D1 between the grating tips facing each other. Assuming that the curved tip planes 9 and 10 in which the grating tips 6b and 7b of the grating portions of the diffraction gratings 6 and 7
5 are ranged are concentric circles, the radius of curvature of the first diffraction grating 6 is defined as $R+D1/2$, and the radius of curvature of the second diffraction grating 7 is defined as $R-D1/2$.

Next, as regards the grating pitch, the grating edge position (zonal radial position) is determined so
10 as to satisfy a desired diffraction condition on the aforementioned imaginary curved surface R. In the case of the concentric circular diffraction optical elements as shown in Figs. 1 and 2, a conical surface
15 perpendicularly intersecting with the imaginary curved surface R at this position is generated, and positions at which this conical surface intersects with the curved tip planes 9 and 10 in which the grating tips of the mountain sides of the respective grating portions
20 are ranged are defined as the grating edge positions of the respective diffraction optical elements. This construction is a construction in which the spacing between the grating portions is kept at a constant value D1 in a direction perpendicularly intersecting
25 with the reference curved surface and the grating edge positions of the respective grating portions are made coincident with each other. On the other hand, the

construction of the embodiment shown in Figs. 1 and 2 wherein the proximate grating tips of the two adjacent grating portions 7-1 and 7-2 are of the same grating pitch distribution and the curved tip planes 9 and 10 in which the grating tips of the respective grating portions are ranged are the same curved surfaces is a construction in which the spacing between the grating portions is kept at a constant value D1 in the direction of the optical axis O and the grating edge positions of the respective grating portions are made coincident with each other. Strictly, the construction shown in Fig. 8 is preferable, but when the spacing D1 between the grating portions is as small as 1-3 μm , there is no great difference between the two, and from the ease of manufacture, the construction shown in Fig. 2 is preferable.

The edge shape of each diffraction grating will now be described. As shown in Fig. 9, design is made such that the angle β formed by the grating edge portions 11a and 11b with respect to the grating surface 6a becomes the same (the edge portion 11a) as or more obtuse (the edge portion 11b) than the angle α formed between a surface normal 11c at a point whereat the curved tip plane 9 and the grating tip 6b intersect with each other and the grating surface 6a, that is, $\alpha \leq \beta$.

Usually, a diffraction optical element, with the

productivity thereof taken into account, is often made by plastic molding or ultraviolet ray setting resin molding by the use of a mold. A molded article having a curved surface shape is generally said to shrink in
5 the direction of a plane perpendicular to the curved surface, and from this, it is preferable to form the grating edge portions 11a and 11b as described previously in order to mold the grating portions with good parting.

10 The grating thickness d_1 (d_2) of each diffraction grating will now be described. In the embodiment of the present invention, design is made such that as shown in Fig. 2, a grating thickness projective component in the direction of a surface normal 11c at a
15 position whereat the curved tip planes 9 and 10 in which the tips of the grating portions are ranged and the grating tips 6b and 7b intersect with each other becomes constant. That is, design is made such that the lengths of the grating edge portions 11a and 11b in
20 a direction parallel to the surface normal become constant.

Fig. 10 shows as a comparative example the cross-sectional shape of a diffraction grating in which the grating thickness parallel to the optical axis O is
25 constant. The cross-sectional shape shown in Fig. 10 is a grating condition under which there is obtained optimum diffraction efficiency when a light beam

entering the diffraction optical element enters substantially in parallelism to the optical axis O. In this case, however, if with the aforescribed moldability taken into account, the grating edge
5 portions 11a and 11b are formed perpendicularly to the reference curved surface R, those of parallel light beams which are indicated by A1 and A2 enter the grating edge portions 11a and 11b, and become unnecessary light beams which are not diffracted in a
10 desired direction of diffraction. Accordingly, to reduce the influence of these unnecessary diffracted lights, it is preferable to use the diffraction optical element so that the light beams may enter the reference curved surface substantially perpendicularly thereto.
15 At this time, the phase difference the diffraction optical element gives to the incident light beams is given from the difference in the length of the optical light path through which the light beams pass.

It is apparent from this that in Fig. 10, the
20 length (ab) of the edge portion 11a in the direction of the optical axis O becomes the grating thickness dab and this is a small grating thickness as compared with the desired grating thickness d1. Therefore, as in the embodiment of the present invention shown in Fig. 2,
25 design is made such that the grating thickness component in the direction of the surface normal 11c of the curved surfaces 9 and 10 at a position whereat the

curved tip planes 9 and 10 in which the tips of the grating portions are ranged and the tips of the grating portions intersect with each other becomes constant, whereby optimum diffraction efficiency is obtained in
5 the use of a diffraction optical element in which the influence of the grating edges is small.

Fig. 3 shows the diffraction efficiency of the diffracted light of the design order of the light beam which has entered the diffraction optical element of
10 the embodiment of the present invention from the direction of a perpendicular to the curved tip planes, and the diffraction efficiency of the diffracted light of the design order of the light beam which has entered the diffraction optical element shown in Fig. 10 from
15 the direction of the optical axis O. It is to be understood here that the grating pitch is 70 μm , the angle formed by and between the surface normal of the reference curved surface and the optical axis is 5°, the material of the diffraction grating 6 of the first
20 diffraction optical element 2 is ultraviolet ray setting resin ($nd = 1.635$, $vd = 23.0$), and the material of the diffraction grating 7 of the second diffraction optical element 3 is ultraviolet ray setting resin C001 ($nd = 1.524$, $vd = 50.8$) produced by Dainippon Chemical Industry Ltd. It is also to be understood that in the
25 respective constructions, the grating thickness d_1 satisfies 6.9 μm and the grating thickness d_2 satisfies

9.5 μm . In Fig. 3, solid line (2) indicates the diffraction optical element of the embodiment of the present invention, and dotted line (1) indicates the diffraction optical element of the construction of Fig.

5 10.

It will be seen from Fig. 3 that the diffraction efficiency of the diffraction optical element of the embodiment of the present invention is high and moreover, performance equal to that of the diffraction 10 optical element of laminated structure formed on a flat surface which is shown in Fig. 22 is obtained.

While the foregoing description has been made of a diffraction optical element in which the curved tip planes are spherical surfaces, the present invention 15 can also be applied to a diffraction optical element in which the curved tip planes are any curved surfaces such as aspherical surfaces, cylindrical surfaces or toric surfaces. The present invention can also be applied to a diffraction optical element having a one-dimensional grating (diffraction grating of equal 20 pitch) as shown in Fig. 11, besides a diffraction optical element having a diffraction grating of which the grating pitch changes gradually.

Fig. 12 is a schematic view of the essential 25 portions of Embodiment 2 of the diffraction optical element of the present invention.

The aforescribed Embodiment 1 has been of a

construction in which the first and second diffraction optical elements are disposed in proximity to each other. Here, it is necessary that the relative positions of the two diffraction optical elements be
5 considerably accurately adjusted to each other. So, Embodiment 2 adopts a construction as shown in Fig. 12 wherein two diffraction optical elements 2 and 3 are adhesively secured to each other in a non-grating area 13 in which the diffraction gratings of the diffraction
10 optical elements 2 and 3 are absent.

By adopting such a construction, the adherence of dust to the surfaces of the gratings can be greatly reduced if the elements are assembled up to the adhesive securing in an environment such as a clean room wherein little dust is present. Also, after the adhesive securing, the surfaces of the gratings are not touched and therefore, the working property when the diffraction optical element 1 is incorporated into other optical system is greatly improved.
15

20 Fig. 13 is a schematic view of the essential portions of Embodiment 3 of the diffraction optical element of the present invention.

The diffraction optical elements of the aforescribed Embodiments 1 and 2 are of a
25 construction in which two diffraction gratings are disposed in proximity to each other. In Embodiment 2, the relative position between the two diffraction

gratings may three-dimensionally cause an error. So, in Embodiment 3, as shown in Fig. 13, portions 14 for regulating the spacing between the grating portions in the direction of height thereof are provided in non-grating areas 13, whereby the relative spacing between the grating portions in the direction of depth thereof is provided with good accuracy.

By such a construction, the alignment of the diffraction gratings may be accomplished by effecting the alignment only in xy directions and the working property is greatly improved. Also, the problem that during alignment, the diffraction gratings interfere with each other and the tips of the gratings are deformed is eliminated. If the portions 14 for regulating the height of the grating portions in the present embodiment are integrally formed of the same material as the material of the diffraction gratings 6 and 7 when the diffraction gratings 6 and 7 are prepared, it will be preferable in both of accuracy and cost. Further, when as shown in Figs. 1, 12 and 13, the substrate has a lens shape, if such adjustment that the relative eccentricity of two lenses is offset is carried out during alignment adjustment, there can be provided a diffraction optical element of good performance in which transmission optical eccentricity is little.

Embodiment 4 of the diffraction optical element of

the present invention will now be described.

While in the diffraction optical elements of the aforescribed embodiments, the materials forming the substrate and the diffraction gratings differ from each other, this is not restrictive, but the material forming the diffraction gratings may be the same as the material of the substrate and the diffraction gratings may be manufactured integrally with the substrate.

By adopting such a construction, the outer diameter of the substrate and the positions of the centers of the diffraction gratings can be adjusted with good accuracy. Or when the substrate has a lens shape, it becomes possible to adjust the core of the substrate lens and the centers of the gratings well. Accordingly, the optical axis adjusting accuracy when the diffraction optical element of the present invention is incorporated into other lens is improved, and the deterioration of an aberration such as imaging performance caused by the element becoming eccentric can be greatly reduced.

Fig. 14 is a schematic view of the essential portions of an optical system using the diffraction optical element according to the present invention.

Fig. 14 shows a cross-section of the photo-taking optical system of a camera or the like, and in Fig. 14, the reference numeral 101 designates a photo-taking lens having a stop 102 and one of the aforescribed

several diffraction optical elements 1 therein. The reference numeral 103 denotes film or a CCD which is an imaging surface.

By using the diffraction optical element according
5 to the present invention, the wavelength dependency of
diffraction efficiency is greatly improved and
therefore, there can be obtained a photo-taking lens of
high performance in which flare is little and the
resolving power at low frequencies is high. Also, this
10 diffraction optical element can be prepared by a simple
manufacturing method and therefore, an inexpensive
optical system excellent in mass productivity as a
photo-taking optical system can be provided.

While in Fig. 14, the diffraction optical element
15 1 of the present invention is provided on the cemented
surface of the fore lens, this is not restrictive, but
the element 1 may be provided on the surface of the
lens, or a plurality of diffraction optical elements
according to the present invention may be used in the
20 photo-taking lens.

Also, in the present embodiment, there has been
shown the case of the photo-taking lens of a camera,
whereas this is not restrictive, but the diffraction
optical element of the present invention can also be
25 used in various imaging optical systems used in a wide
wavelength range, such as the photo-taking lens of a
video camera, the image scanner of a business machine

and the reader lens of a digital copier to thereby obtain a similar effect.

Fig. 15 is a schematic view of the essential portions of an optical system using the diffraction optical element according to the present invention.

Fig. 15 shows a cross-section of the observation optical system of binoculars or the like, and in Fig. 15, the reference numeral 1 designates an objective lens including one of the diffraction optical elements of the aforescribed embodiments, and the reference numeral 104 denotes image reversing means such as a poroprism for forming an image, and in Fig. 15, it is shown as a glass block for the sake of simplicity. The reference numeral 105 designates an eyepiece, and the reference numeral 106 denotes an evaluation plane (pupil plane). The diffraction optical element 1 is formed with a view to correct the chromatic aberration or the like on the imaging plane 103 of the objective lens.

By using the diffraction optical element according to the present invention, the wavelength dependency of diffraction efficiency is greatly improved and therefore, there can be obtained an objective lens of high performance in which flare is little and the resolving power at low frequencies is high. Also, the diffraction optical element of the present invention can be prepared by a simple manufacturing method and

therefore, there can be provided an inexpensive optical system excellent in mass productivity as an observation optical system.

While in the present embodiment, there has been
5 shown a case where the diffraction optical element is formed on the objective lens portion, this is not restrictive, but a similar effect may be obtained even if the diffraction optical element is formed on the surface of the prism or at a position in the eyepiece.
10 However, by the diffraction optical element being provided more adjacent to the object side than the imaging plane, there is the chromatic aberration reducing effect by only the objective lens and therefore, in the case of an observation system for the
15 naked eye, it is desirable to provide the diffraction optical element at least on the objective lens side.

Also, the optical system of the present embodiment has been shown as binoculars, whereas this is not restrictive, but it may be an optical system such as a
20 ground telescope or an astronomical telescope, and the present invention can also be applied to an optical system such as the optical type finder of a lens shutter camera, a video camera or the like to thereby obtain an effect similar to that in the case of
25 binoculars.